Dynamics of ULVZ-mantle interaction using fast multipole boundary element method NSF EAR 0911094 and EAR 1215800

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The UltraLow Velocity Zones

- 3:1 s-wave to p-wave loss in velocity
- 50-100 km wide
- 10-40 km thick
- 1-2 orders of magnitude less viscous
- 10% more dense
- Dynamically coupled to surrounding mantle



[McNarama et al. 2010]



[Garnero and McNarama 2008]

Experimental Model

- Forcing terms
 - Buoyancy
 - Imposed velocity field (flow within LLSVP)
- Modulating terms
 - Viscosity ratio varies patches desire to deform
- Patch interaction



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What is the drainage rate of the ULVZ?

 The Stokes Boundary Integral Equation (BIE) for multiple domains [Pozrikidis 2001]

$$\frac{1+\lambda_q}{2}u_j(\boldsymbol{x}) = u_j^{\infty}(\boldsymbol{x}_0) - \sum_{p=1}^{P} \frac{\mathcal{R}_p}{4\pi} \int_{\Gamma_p} \Delta f_i^{(p)}(\boldsymbol{x}) U_{ij}(\boldsymbol{x}, \boldsymbol{x}_0) \,\mathrm{d}\Gamma_m(\boldsymbol{x})$$

 $+\sum_{p=1}^{P} \frac{1-\lambda_p}{4\pi} \int_{\Gamma_p}^{\mathcal{P}\mathcal{V}} u_i(\boldsymbol{x}) T_{ijk}(\boldsymbol{x}, \boldsymbol{x}_0) \hat{n}_k(\boldsymbol{x}) \,\mathrm{d}\Gamma_p(\boldsymbol{x})$

The interfacial surface term is buoyancy driven

$$\mathcal{R}^{(p)} = \frac{(\rho_m - \rho_p)gx_c^2}{u_c\mu_m}$$

 $\lambda_p = \frac{\mu_p}{\mu_m}$

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Numerical Method

- Collocation
- Cubic spline interpolation for geometry
- Gaussian quadrature or RIM2D (singular) integration
- Generally dense and asymmetric





Fast Multipole Method

- Approximate the integral over a boundary element
- Move series expansions up and down a tree
 - Translate
 - Combine
- Distant interactions represented by a series
- Nearby interactions are computed directly



Direct Method

• Tree structure results in $\mathcal{O}(N \log N)$ iterative method

Fast Multipole Method

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Fast Method

• Tree structure results in $\mathcal{O}(N \log N)$ iterative method

ULVZ Simulation #1 Buoyancy Driven System No Imposed Velocity



ULVZ Dynamics (5 Myrs)

Left: High patch viscosity, low buoyancy force Right: Low patch viscosity, high buoyancy force

Patch Settling



Patch Settling



Patch Settling



ULVZ Simulation #2 Upwell Driven Imposed Flow



Upwell Dynamics (10 Myrs) Left: High patch viscosity

Right: Low patch viscosity

Summary

- Numerically experimented via FMBEM the ULVZ patch drainage in LLSVP for various densities and viscosities
- Inverse linear relationship between viscosity and drainage rate
- Linear relationship between compositional Rayleigh number and drainage rate
- Interaction of patches leads to asymmetric spreading
- Evidence of core deformation for ULVZ-like parameters

References

- X. Gao, "Numerical evaluation of two-dimensional singular boundary integrals--Theory and Fortran code", <u>Journal of Computational and Applied Mathematics</u>, Volume 118, Pages 44-64, 2006
- E.J. Garnero and A.K. McNamara, "Structure and Dynamics of Earth's Lower Mantle", <u>Science</u>, Volume 320, Issue 5876, Pages 626-628, 2008
- S. Hier-Majumder and J. Revenaugh, "Relationship between the viscosity and topography of the ultralow-velocity zone near the core-mantle boundary", <u>Earth and Planetary Science</u> <u>Letters</u>, Volume 299, Pages 382-386, 2010
- D.M. Koch and D.L. Koch, "Numerical and theoretical solutions for a drop spreading below a free fluid surface", <u>Journal of fluid mechanics</u>, Volume 287, Issue 1, Pages 251-278, 1994
- L.G. Leal, <u>Advanced Transport Phenomena: Fluid Mechanics and Convective Transport</u> <u>Processes</u>, Cambridge Series in Chemical Engineering, 2007
- T.M. Lassak et al., "Core-mantle boundary topography as a possible constraint on lower mantle chemistry and dynamics", <u>Earth and Planetary Science Letters</u>, Volue 289, Pagrs 232-241, 2010
- Y.J. Liu and N. Nishimura, "The fast multipole boundary element method for potential problems: a tutorial", <u>Engineering Analysis with Boundary Elements</u>, Volume 30, Issue 2, Pages 371-381, 2006

References

- Y.J. Liu, "A new fast multipole boundary element method for solving 2-D Stokes flow problems based on a dual BIE formulation", <u>Engineering Analysis with Boundary Elements</u>, Volume 32, Issue 2, Pages 139-151, 2008
- M. Manga and H.A. Stone, "Buoyancy-Driven Interactions Between 2 Deformable Viscous Drops", <u>Journal of fluid mechanics</u>, Volume 256, Pages 647-683, 1993
- A.K. McNamara, E.J. Garnero, and S. Rost, "Tracking deep mantle reservoirs with ultra-low velocity zones", <u>Earth and Planetary Science Letters</u>, Volume 299, Pages 1-9, 2010
- C. Pozrikidis, <u>Boundary integral and singularity methods for linearized viscous flow</u>, Cambridge Texts in Applied Mathematics, 1992
- C. Pozrikidis, "Interfacial Dynamics for Stokes Flow", <u>Journal of Computational Physics</u>, Volume 169, Issue 2, Pages 250-301, 2001
- S. Rost et al., "Seismological constraints on a possible plume root at the core-mantle boundary", <u>Nature</u>, Volume 435, Issue 7042, Pages 666-669, 2005
- M.S. Warren and J.K. Salmon, "A Parallel Hashed Oct-Tree N-Body Algorithm", <u>Proceedings of the 1993 ACM/IEEE conference on Supercomputing</u>, AMC, Pages 12-21, 1993

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Extra Slides FMM Expansions

Validity of Expansion

- Expansions are valid based on the L₂ distance between boundary elements and Greens functions
- Distance matrices cost O(N²) time and space to compute
- Approximate distances using *L*₁ norm to determine areas of validity

x=0.01010101110 y=0.10111010100 01100111011001

 A Morton number scheme is used to greatly accelerate the process [Warren 1993]











Extra Slides CMB 4x4 Simulation

Settling Interaction

- Two ULVZ patches are placed above a core
 - The viscosity ratio and density contrast of the patches with respect to the mantle is varied
 - The viscosity ratio parameter ranges from 1e-2 to 1
 - The density of the patches are varied 2-8% more dense than the mantle
 - Simulations are run for 5 million years



Extra Slides Imposed Flow Simulation

Rising Interaction

- Two patches are placed in an upswell imposed velocity similar to a plume.
 - The viscosity ratio and density contrast of the patches with respect to the mantle is varied
 - The viscosity ratio parameter ranges from 1e-2 to 1
 - The density of the patches is varied between 102% and 110% of mantle density
 - Simulations are run for 5 million years

Rising Analysis

- For low compositional Rayleigh number, solution is dominated by the imposed velocity field
- For moderately size compositional Rayleigh numbers the upswell is able to support some or all of the patch
- With large compositional Rayleigh numbers the density contrast of the patch overcomes the imposed velocity
- For all compositional Rayleigh numbers low viscosity ratios allows the patch to deform easily in the direction of greatest velocity



Patch Interaction

- Velocity is able to uplift part of the particles
- In low velocity regions, gravitational force
 overcomes
- As particles approach, pressure builds and velocities repel
- No spreading due to lack of lower boundary



Extra Slides Evidence Of Core Deformation



[Lassak et al. 2010]

Numerical model of core mantle boundary shows deformation in areas of detected ULVZs.